


Determination of K

Having known the K-G relation, the next question to answer is how to determine K for a given elasticity problem.

Answer: Use stresses in front of the crack tip or the crack opening or shearing/sliding displacements behind the crack tip.


$$\left. \begin{aligned} K_I &= \lim_{r \rightarrow 0} \sqrt{2\pi r} \sigma_{yy}(r, \theta=0) \\ K_{II} &= \lim_{r \rightarrow 0} \sqrt{2\pi r} \sigma_{xy}(r, \theta=0) \\ K_{III} &= \lim_{r \rightarrow 0} \sqrt{2\pi r} \sigma_{yz}(r, \theta=0) \end{aligned} \right\} \begin{array}{l} \leftarrow \text{True for both} \\ \text{isotropic \& } \\ \text{anisotropic} \\ \text{materials} \end{array}$$

or

$$\left\{ \begin{aligned} K_I &= \lim_{r \rightarrow 0} \frac{E'}{8} \sqrt{\frac{2\pi}{r}} [u_y(r, \theta=\pi) - u_y(r, \theta=-\pi)] \\ K_{II} &= \lim_{r \rightarrow 0} \frac{E'}{8} \sqrt{\frac{2\pi}{r}} [u_x(r, \theta=\pi) - u_x(r, \theta=-\pi)] \\ K_{III} &= \lim_{r \rightarrow 0} \frac{\mu}{4} \sqrt{\frac{2\pi}{r}} [u_z(r, \theta=\pi) - u_z(r, \theta=-\pi)] \end{aligned} \right.$$

True only for isotropic materials

Then the rest would be to solve for u or \underline{q} from (mixed) boundary value problem with given geometry and boundary conditions. Accordingly, we can apply methods such as separation of variables, transform method, Wiener-Hopf technique,

Green's function, conformal mapping, complex variable method, and DNS.

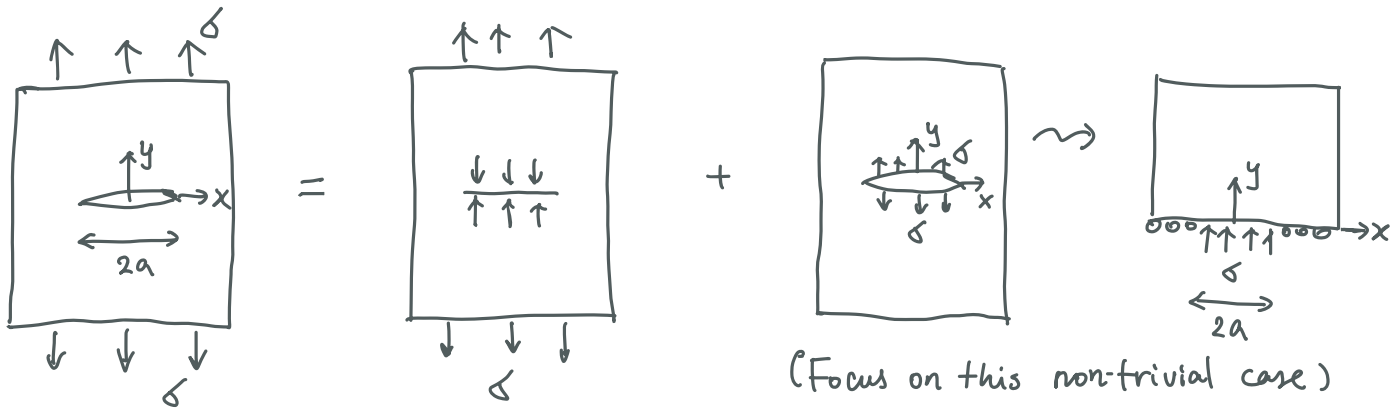
used later

limited success

will be used extensively

\leftarrow To deal with non-vanishing ends

Let's consider the center crack problem again but solve it by transform method.



Governing equation: $\nabla^2 \nabla^2 \phi = 0$ ($= \nabla^4 u = \nabla^4 v$)

Boundary conditions: $\tau_{xy} = 0$ on $y=0$, $\sigma_{yy} = -\sigma$ on $y=0$, $|x| < a$

$v = 0$ on $y=0$, $|x| > a$

all terms $\rightarrow 0$ as $y \rightarrow \infty$

Fourier transform: $\tilde{f}(k) = \int_{-\infty}^{\infty} f(x) e^{ikx} dx = H(f)$

Inverse FT: $f(x) = \frac{1}{2\pi} \int_{-\infty}^{\infty} \tilde{f}(k) e^{-ikx} dk = H^{-1}(f)$

Property: $\int_{-\infty}^{\infty} \frac{df}{dx} e^{ikx} dx = f e^{ikx} \Big|_{-\infty}^{\infty} - ik \int_{-\infty}^{\infty} f e^{ikx} dx \rightarrow \tilde{f}' = -ik \tilde{f}$

$\rightarrow H(\nabla^2(\nabla^2 \phi)) = \left(\frac{d^2}{dy^2} - k^2\right)^2 \tilde{\phi} = 0$

The solution can be written in the form

$\tilde{\phi}(k, y) = (A + By) e^{-|k|y} + (C + Dy) e^{+|k|y}$

To determine integration constants, we need to obtain expression of stresses and displacements in term of $\tilde{\phi}$.

$$\tilde{\sigma}_{xx} = \int_{-\infty}^{\infty} \sigma_{xx} e^{ikx} dx = \int_{-\infty}^{\infty} \frac{\partial^2 \phi}{\partial y^2} e^{ikx} dx = \frac{\partial^2 \tilde{\phi}}{\partial y^2}$$

$$\tilde{\sigma}_{yy} = \int_{-\infty}^{\infty} \frac{\partial^2 \phi}{\partial x^2} e^{ikx} dx = -k^2 \tilde{\phi}$$

$$\tilde{\sigma}_{xy} = \int_{-\infty}^{\infty} -\frac{\partial^2 \phi}{\partial x \partial y} e^{ikx} dx = +ik \frac{\partial \tilde{\phi}}{\partial y}$$

As $y \rightarrow \infty$, $\sigma_{ij} \rightarrow 0 \rightarrow C = D = 0$

At $y=0$, $\sigma_{yy} = -p(x) \Rightarrow -k^2 \tilde{\phi}|_{y=0} = -Ak^2 = -\tilde{p}(k) \rightarrow A = \tilde{p}(k)/k^2$
Arbitrary even function ↖ even function of k

$$\sigma_{xy} = 0 \Rightarrow \frac{\partial \tilde{\phi}}{\partial y} \Big|_{y=0} = -|k|A + B = 0 \rightarrow B = \tilde{p}(k)/|k|$$

$$\rightarrow \tilde{\phi} = \frac{\tilde{p}(k)}{k^2} (1 + |k|y) e^{-|k|y}$$

$$\tilde{\sigma}_{xx} = -\tilde{p} (1 - |k|y) e^{-|k|y}$$

$$\tilde{\sigma}_{yy} = -\tilde{p} (1 + |k|y) e^{-|k|y}$$

$$\tilde{\sigma}_{xy} = -i\tilde{p} ky e^{-|k|y}$$

↑ odd of k

Once we know $p(x)$, we can calculate $\tilde{p}(k)$ and then $\tilde{\sigma}_{ij}$ & σ_{ij} . While $p(x) = 0$ for $|x| < a$, $p(x)$ for $|x| > a$ is also part of the solution to ensure $v(x) = 0$. We then need expressions for \tilde{u} and \tilde{v} as well.

$$\epsilon_x = \frac{\partial u}{\partial x} = \frac{1}{E'} (\sigma_{xx} - \nu' \sigma_{yy}) \rightarrow -ik \tilde{u} = \frac{1}{E'} (\tilde{\sigma}_{xx} - \nu' \tilde{\sigma}_{yy}) \quad (30)$$

$$\rightarrow \tilde{u} = \frac{i\tilde{p}}{E'k} \left[-(1-\nu') + (1+\nu')|k|y \right] e^{-|k|y}$$

\leftarrow Odd function of k [Typo in Sneddon's book]

$$\epsilon_{xy} = \frac{1}{2} \left(\frac{\partial u}{\partial y} + \frac{\partial v}{\partial x} \right) = \frac{1+\nu'}{E'} \sigma_{xy} \rightarrow \frac{\partial \tilde{u}}{\partial y} - ik \tilde{v} = \frac{2(1+\nu')}{E'} \tilde{\sigma}_{xy}$$

$$\rightarrow \tilde{v} = \frac{\tilde{p}}{E'|k|} \left[2 + (1+\nu')|k|y \right] e^{-|k|y}$$

\leftarrow Even function of k

We are particularly interested in σ_{yy} and v , associated with which BCs are.

$$\sigma_{yy} = \frac{-1}{2\pi} \int_{-\infty}^{\infty} \underbrace{\tilde{p}(1+|k|y)}_{\text{Even of } k} e^{-|k|y} e^{-ikx} dk = -\frac{1}{\pi} \int_0^{\infty} \tilde{p}(1+ky) e^{-ky} \cos kx dk$$

$$v = \frac{1}{2\pi} \int_{-\infty}^{\infty} \frac{\tilde{p}}{E'|k|} \left[2 + (1+\nu')|k|y \right] e^{-|k|y} e^{-ikx} dk = \frac{1}{\pi E'} \int_0^{\infty} \tilde{p} \left[2 + (1+\nu')ky \right] e^{-ky} \frac{\cos kx}{k} dk$$

On the surface of $y=0$, we have

$$\sigma_{yy} = -\frac{1}{\pi} \int_0^{\infty} \tilde{p}(k) \cos kx dk, \quad v(x) = \frac{2}{\pi E'} \int_0^{\infty} \tilde{p}(k) \frac{\cos kx}{k} dk$$

We see therefore that the equations determining $\tilde{p}(k)$ are the dual integral equations.

$$\frac{2}{\pi} \int_0^{\infty} \tilde{p}(k) \cos kx dk = p(x), \quad 0 \leq x \leq a$$

$$\int_0^{\infty} \tilde{p}(k) \frac{\cos kx}{k} dk = 0, \quad x > a$$

The dual integral equations (often in mixed BVP) need to be solved numerically in general.

However, for this problem, we can make use of Busbridge's solution.

$$K = k \cdot a, \quad x = x/a, \quad \tilde{P} = \tilde{P}/K^{1/2}, \quad P = a \left(\frac{\pi}{2x}\right)^{1/2} p_0, \quad \cos kx = \left(\frac{\pi Kx}{2}\right)^{1/2} J_{-1/2}(Kx)$$

$$\rightarrow \begin{cases} \int_0^\infty K \tilde{P}(K) J_{-1/2}(Kx) dK = P(x), & 0 \leq x \leq 1 \\ \int_0^\infty \tilde{P}(K) J_{-1/2}(Kx) dK = 0, & x > 1 \end{cases}$$

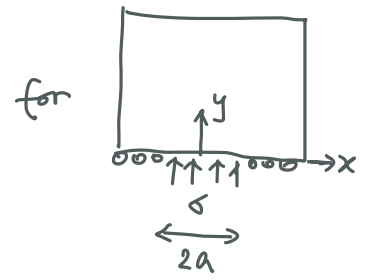
Sneddon showed the solution (Page 424)

$$\tilde{P}(K) = \left(\frac{2K}{\pi}\right)^{1/2} \left[J_0(K) \int_0^1 x^{1/2} (1-x^2)^{1/2} P(x) dx + K \int_0^1 x^{1/2} (1-x^2)^{1/2} dx \int_0^1 P(\alpha x) \alpha^{5/2} J_1(K\alpha) d\alpha \right]$$

When $p(x) = \sigma$ within $|x| < 1$, $\tilde{P}(K) = \frac{1}{2} \pi \sigma a J_1(ka)$

$$v(y=0) = \frac{2}{E'} \sigma (a^2 - x^2)^{1/2}$$

$$\sigma_{yy}(y=0, x > c) = \sigma \left[\frac{x}{(x^2 - a^2)^{1/2}} \right]$$



for the problem by adding the trivial solution.

We then can calculate the stress intensity factor by

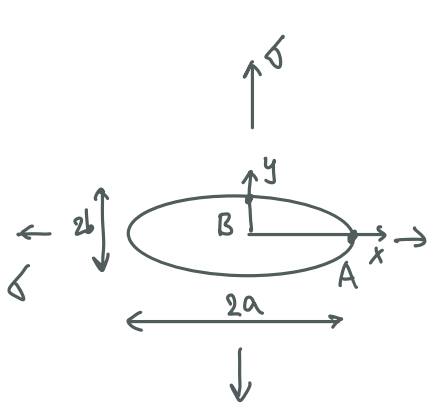
$$K_I = \lim_{r \rightarrow 0} \sqrt{2\pi r} \sigma_{yy}(r, \theta=0) \stackrel{x=r+a}{=} \lim_{r \rightarrow 0} \sqrt{2\pi r} \sigma \cdot \frac{r+a}{\sqrt{(r+a)^2 - a^2}} = \sqrt{\pi a} \sigma$$

or

$$K_I = \lim_{r \rightarrow 0} \frac{E'}{8} \sqrt{\frac{2\pi}{r}} u_y(r, \theta=\pi) \times 2 \stackrel{x=a-r}{=} \lim_{r \rightarrow 0} \frac{E'}{4} \sqrt{\frac{2\pi}{r}} \cdot \frac{2}{E'} \sigma \sqrt{2a+r} \sqrt{r} = \sqrt{\pi a} \sigma$$

↑
Symmetry

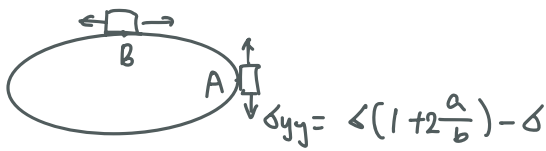
For this problem, the crack opening displacement can also be calculated by considering the following problem:



(Taking $b \rightarrow 0$ gives rise to a center crack).

Eshelby: The strain in an ellipsoidal inclusion in an infinite matrix loaded at infinity is uniform.

$$\sigma_{xx} = \sigma \left(1 + 2 \frac{b}{a}\right) - \sigma$$



$$\sigma_{yy} = \sigma \left(1 + 2 \frac{a}{b}\right) - \sigma$$

- From elasticity we know the stress concentration at 2 key points

- Thinking of the void as an "inclusion" with shear modulus $\mu \rightarrow 0$

Using strain continuity conditions at the edge of the void, we can determine the "strain" in the void, i.e.,

$$\epsilon_{yy}^{void} = \epsilon_{yy}^{A/void} = \epsilon_{yy}^{A/matrix} = \frac{2\sigma}{E'} \frac{a}{b} \quad \left(\text{since } \sigma_{xx}^{A/void} = \sigma_{xx}^{A/matrix} = 0 \right)$$

$$\epsilon_{xx}^{void} = \epsilon_{xx}^{B/void} = \epsilon_{xx}^{B/matrix} = \frac{2\sigma}{E'} \frac{b}{a} \quad \left(\sigma_{yy}^{A/void} = \sigma_{yy}^{A/matrix} = 0 \right)$$

$$\epsilon_{xy}^{void} = 0 \quad (\text{symmetry})$$

Then the displacement field of the void is

$$u_x = \epsilon_x^{void} \cdot x = \frac{2\sigma}{E'} \frac{b}{a} x, \quad u_y = \epsilon_y^{void} \cdot y = \frac{2\sigma}{E'} \frac{a}{b} y$$

• The vertical displacement "COD" on the surface $(\frac{x}{a})^2 + (\frac{y}{b})^2 = 1$, where

$$y = \pm b \sqrt{1 - (\frac{x}{a})^2}$$

→ on the surface $u_y = \pm \frac{2\delta}{E'} \sqrt{a^2 - x^2}$, $u_x = \frac{2\delta}{E'} \frac{b}{a} x$

→ Now take $b \rightarrow 0$ $u_y = \pm \frac{2\delta}{E'} \sqrt{a^2 - x^2}$, $u_x = 0$

$$COD(x) = \frac{4\delta}{E'} \sqrt{a^2 - x^2}$$

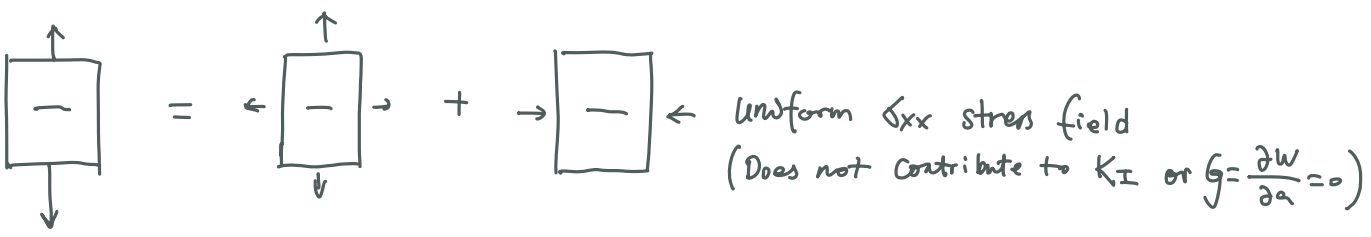


$$K_I = \lim_{r \rightarrow 0} \frac{E'}{8} \sqrt{\frac{2\pi}{r}} COD(x) \stackrel{x=a-r}{=} \lim_{r \rightarrow 0} \frac{E'}{4} \sqrt{\frac{2\pi}{r}} \cdot \frac{2}{E'} \delta \sqrt{2a+r} \sqrt{r} = \sqrt{\pi a} \delta$$

Then what about



K_I ?



uniform σ_{xx} stress field
(Does not contribute to K_I or $G = \frac{\partial W}{\partial a} = 0$)

$$K_I = \sqrt{\pi a} \delta + (K_I = 0) = \sqrt{\pi a} \delta$$

This is nice for a simple problem, but what about more general methods?